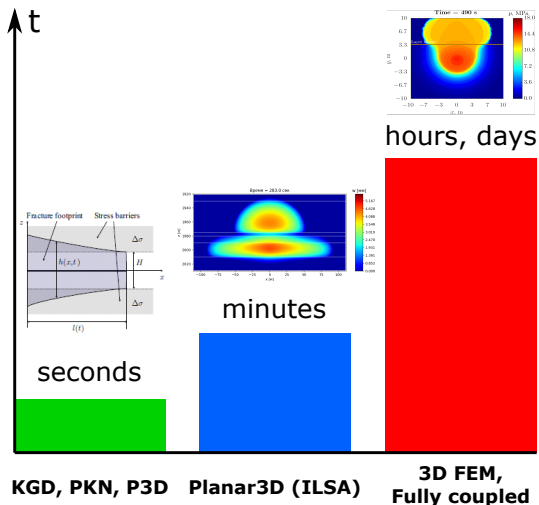


# Poroelectric effects influence range for radial hydraulic fracturing model

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FRAC2019, Novosibirsk

# Fracturing Simulation Time

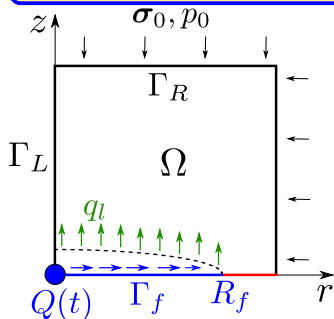
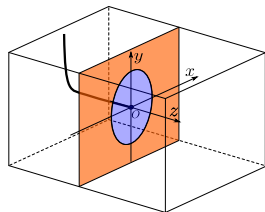


# Problem Formulation

## Biot's equations of poroelasticity

$$\operatorname{div} \boldsymbol{\sigma} = 0, \quad \boldsymbol{\sigma} = \underbrace{\lambda \operatorname{div} \vec{u} \mathbf{I} + 2\mu \boldsymbol{\mathcal{E}}(\vec{u})}_{\text{Elastic Stress}} - \underbrace{\alpha p \mathbf{I}}_{\text{Pore Pressure}}$$

$$S_\varepsilon \frac{\partial p}{\partial t} = \operatorname{div} \left( \frac{k_r}{\eta_r} \nabla p - \alpha \frac{\partial \vec{u}}{\partial t} \right)$$



$$\Gamma_R : p = p_0, \quad \boldsymbol{\sigma} \langle \vec{n} \rangle = -\sigma_\infty \vec{n}$$

$$\Gamma_L : \frac{\partial u_z}{\partial r} = 0, \quad u_r = 0, \quad \frac{\partial p}{\partial r} = 0$$

$$\Gamma_f : \boldsymbol{\sigma} \langle \vec{n} \rangle = -(p - \sigma_{coh}) \vec{n}, \quad u_z \geq 0$$

$$\Gamma_f : \frac{\partial d}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{d^3}{12\eta_f} \frac{\partial p}{\partial r} \right) + \frac{k_r}{\eta_r} \frac{\partial p}{\partial z} + \frac{Q(t)}{2\pi r} \delta(r), \quad d = 2u_z.$$

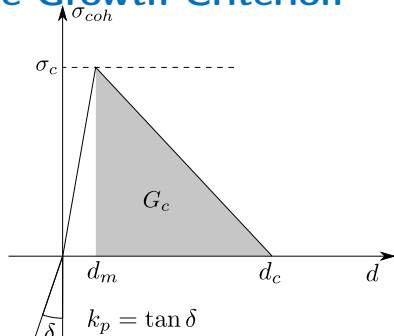
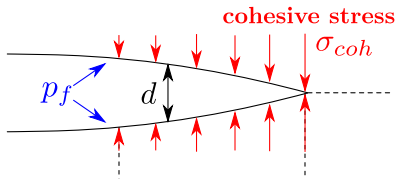
## Solution Method: Weak Formulation

$$\int_{\Omega} (\lambda \operatorname{div}(\vec{u}) - \alpha p) \operatorname{div}(\vec{\psi}) + 2\mu \mathcal{E}(\vec{u}) : \mathcal{E}(\vec{\psi}) r \, dr dz$$
$$- \int_{\Gamma_f} (p - \sigma_{coh} - \sigma_0) \psi_z r \, dr = 0, \quad \sigma_0 = \sigma_{\infty} - p_0,$$
$$\int_{\Omega} S_{\varepsilon} \frac{\partial \mathbf{p}}{\partial \mathbf{t}} \varphi r \, dr dz + \int_{\Omega} \frac{k_r}{\eta_r} \nabla p \cdot \nabla \varphi r \, dr dz + \int_{\Omega} \alpha \frac{\partial}{\partial t} (\operatorname{div} \vec{u}) \varphi r \, dr dz +$$
$$+ \int_{\Gamma_f} \frac{\partial \mathbf{u}_z}{\partial \mathbf{t}} \varphi r \, dr + \int_{\Gamma_f} \frac{\mathbf{u}_z^3}{3\eta_f} \frac{\partial p}{\partial r} \frac{\partial \varphi}{\partial r} r \, dr dz = \frac{\mathbf{Q}(\mathbf{t})}{4\pi} \varphi(0, 0).$$

$$\Gamma_L : \quad \psi_r = 0, \quad u_r = 0$$
$$\Gamma_R : \quad \varphi = 0, \quad p = 0$$

**Solve via  
Finite Element Method**

# Solution Method: Fracture Growth Criterion



$$+ \int_{\Gamma_f} \sigma_{coh}(2u_z^{k+1}) \psi_z r dr \approx$$

$$\int_{\Gamma_f} \left( \sigma_{coh}(2u_z^k) + 2 \frac{\partial \sigma_{coh}}{\partial (2u_z)} (2u_z^k) (u_z^{k+1} - u_z^k) \right) \psi_z r dr$$

## Reference Simulation Parameters

Parameter	Value
Young's Modulus, $E$	20 GPa
Poisson's Ratio, $\nu$	0.24
Reservoir Permeability, $k_r$	$10^{-16}$ – $10^{-13}$ m <sup>2</sup>
Storativity, $S_\epsilon$	$10^{-11}$ – $10^{-8}$ Pa <sup>-1</sup>
Biot Coefficient, $\alpha$	0, 0.75
Closure Stress, $\sigma_0$	1–100 MPa
Reservoir Fluid Viscosity, $\eta_r$	$10^{-2}$ Pa · s
Fracture Fluid Viscosity, $\eta_f$	$10^{-2}$ – $10^{-1}$ Pa · s
Pumping rate, $Q$	$5 \times 10^{-2}$ m <sup>3</sup> /s

# 1D Filtration process

Adopting  $\sigma_{zz} = (\lambda + 2\mu)\varepsilon_{zz} - \alpha p$

$$S_t \frac{\partial p}{\partial t} = \frac{\partial}{\partial z} \left( \frac{k_r}{\eta_r} \frac{\partial p}{\partial z} \right) - \frac{\alpha}{\lambda + 2\mu} \frac{\partial \sigma_{zz}}{\partial t}, \quad S_t = S_\varepsilon + \varkappa \frac{\alpha^2}{\lambda + 2\mu}, \quad (1)$$

Boundary and initial conditions:

$$p|_{t=0} = 0, \quad p|_{z=0} = P = \text{const} \quad (2)$$

Solution

$$p(t, z) = P \cdot \text{erfc} \left( \frac{z}{\ell_d(t)} \right), \quad c = \frac{k_r}{\eta_r S_t}$$

Diffusion length

$$\ell_d(t) = \sqrt{4ct}.$$

Carter formula

$$q_l = - \left. \frac{k_r}{\eta_r} \frac{\partial p}{\partial z} \right|_{z=0} = \frac{C_L}{\sqrt{t}}, \quad C_L = P \sqrt{\frac{k_r}{\pi \eta_r} S_t}, \quad (3)$$

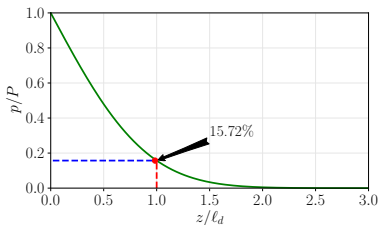
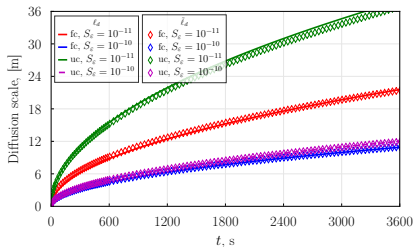
higher **storativity**  $\Rightarrow$  higher **leak-off**, but smaller **diffusion scale**  $\ell_d$ .

# 1D Filtration Process

At point  $z = \ell_d(t)$  pressure is dropped down to 15.72 % of the boundary level  $P$ . **Generalized diffusion scale:**

$$\tilde{\ell}_d(t) = \inf\{z : p(t, z) \leq 0.1572 p(t, 0)\}$$

$$\ell_d(t) = \sqrt{4ct}$$



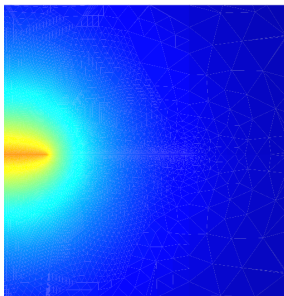
**Figure:** Diffusion scales for fully coupled (fc)  $\alpha_e = \alpha_f = 0.75$  and uncoupled cases  $\alpha_e = \alpha_f = 0.0$ .

**Other params:**  $k_r = 10^{-14} \text{ m}^2$ ,  $\sigma_0 = 10 \text{ MPa}$ ,  $\eta_f = 0.01 \text{ Pa}\cdot\text{s}$

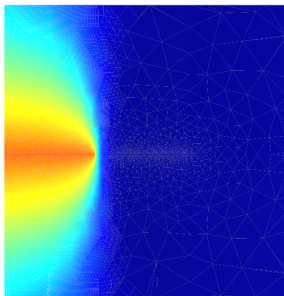


# 1d vs 3d diffusion

a - 2D diffusion



b - 1D diffusion



-1.84e+05    4.69e+06    9.57e+06

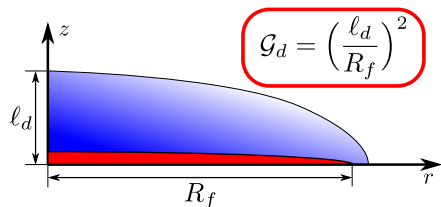


[Carrier, Granet, 2012]

- ▶  $\int_{\Omega} \frac{k_r}{\eta_r} \left( \frac{\partial p}{\partial z} \frac{\partial \varphi}{\partial z} + \kappa \frac{\partial p}{\partial r} \frac{\partial \varphi}{\partial r} \right) r dr dz, \quad \kappa = 10^{-5} - \text{anisotropic filtr. eq.}$
- ▶ Fracture front is **faster** than diffusion:  $\ell_d \ll R_f$

# 1D to 3D diffusion transition

$\mathcal{G}_d^{crit} \approx 0.2 \Rightarrow$  fracture is 2.23 times faster than filtration front



## 1D vs 3D filtration

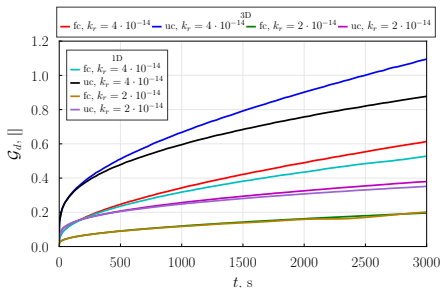


Figure: Diffusion dimensionless complex  $\mathcal{G}_d$  in case of **3D diffusion** ( $\kappa = 1$ ) and **1D diffusion** ( $\kappa = 10^{-5}$ ) for fully coupled (fc) and uncoupled (uc) cases and different permeability ( $k_r = 2 \times 10^{-14} \text{ m}^2$  and  $k_r = 4 \times 10^{-14} \text{ m}^2$ ).

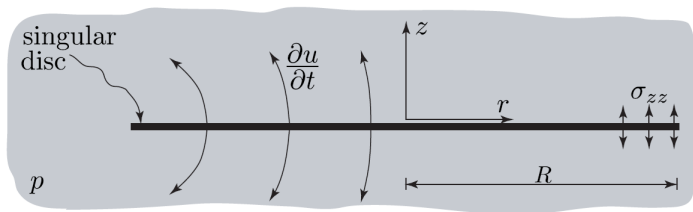
Other params:  $S_\varepsilon = 10^{-11} \text{ Pa}^{-1}$ ,  $\sigma_0 = 10 \text{ MPa}$ ,  $\eta_f = 0.1 \text{ Pa}\cdot\text{s}$

# Backstress Green's functions

For constant pressure [Kovalyshen, 2010]

$$\sigma_b(t, r) = \int_0^t S_b(R_f(s), r, t - s) p(s) ds,$$

$S_b(R_f, r, t)$  — **vertical stress**  $\sigma_{zz}$  generated by **instantaneous unit pressure impulse** along disk  $\{r \leq R_f, z = 0\}$ .



## Backstress dimensionless complex

Scaling:

$$\sigma_b(t, r) = (p^*(t) - \sigma_0)\Sigma(t, r), \quad S_b(R_f, r, t) = \frac{\eta}{T_{R_f}} \Xi\left(\frac{r}{R_f}, \frac{t}{T_{R_f}}\right),$$

$$T_{R_f} = \frac{R_f^2}{4c}, \quad \eta = \alpha \frac{1 - 2\nu}{2 - 2\nu}, \quad \mathcal{G}_d(t) = \frac{\ell_d^2(t)}{R_f^2(t)},$$

$$\Sigma(t, s) = \mathcal{G}_{bs}(t) \int_0^1 \frac{R_f^2(t)}{R_f^2(ts)} \Xi\left(\frac{r}{R_f(ts)}, \mathcal{G}_d(1-s) \frac{R_f^2(t)}{R_f^2(ts)}\right) \frac{p^*(ts)}{p^*(t)} ds,$$

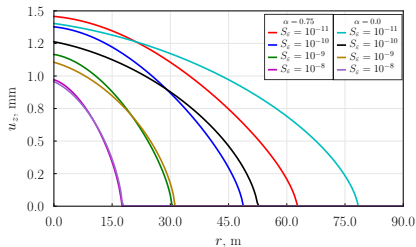
$$\mathcal{G}_{bs}(t) = \eta \mathcal{G}_d(t) \left(1 + \frac{\sigma_0}{p^*(t) - \sigma_0}\right)$$

$p^*(t)$  – mean pressure value

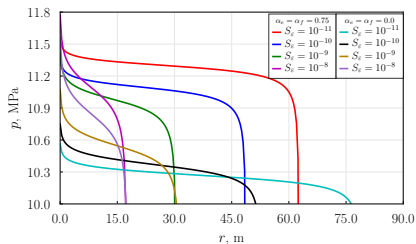
**Backstress  
dimensionless  
complex**

# Poroelastic effects

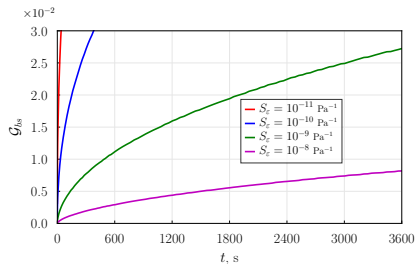
Half-width at  $t = 1404$  s



Pressure at  $t = 1404$  s

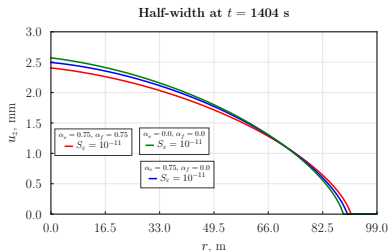


$$g_{bs}^{crit} = 10^{-3}$$

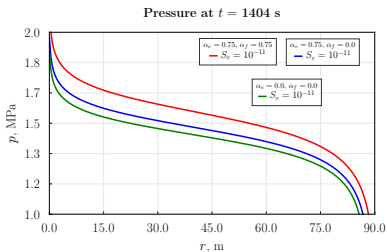


Param.	Value
$k_r$	$10^{-14}$ m $^2$
$\sigma_0$	10 MPa
$\eta_f$	$10^{-2}$ Pa $\cdot$ s

# Deformation domination



(a)



(b)

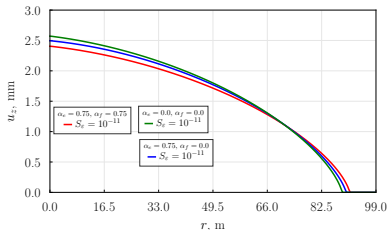
Param.	Value
$k_r$	$10^{-15} \text{ m}^2$
$\sigma_0$	1 MPa
$\eta_f$	$10^{-1} \text{ Pa} \cdot \text{s}$

$$C_L = \sigma_0 \sqrt{\frac{k_r}{\pi \eta_r}} S_t \approx 10^{-6} \text{ m} / \sqrt{\text{s}}$$

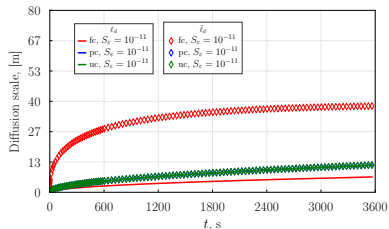
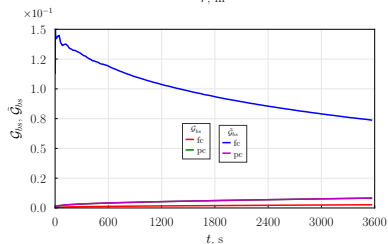
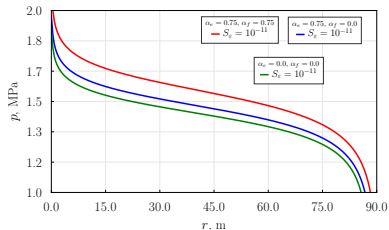
almost **Storage-viscosity regime**

# Deformation domination

Half-width at  $t = 1404$  s



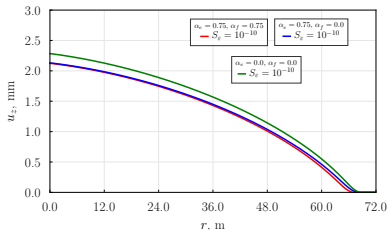
Pressure at  $t = 1404$  s



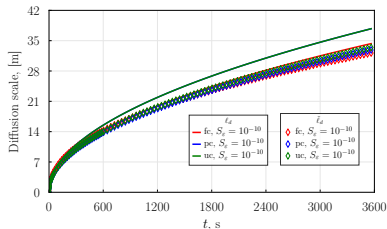
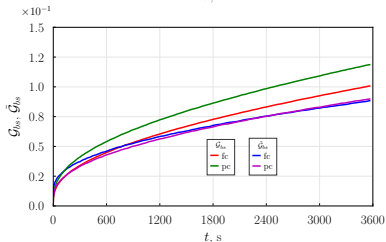
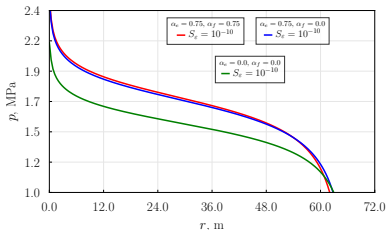
$\tilde{G}_d(t)$  reflects pressure diffusion better

# Deformation domination (weak effect)

Half-width at  $t = 1404$  s



Pressure at  $t = 1404$  s



Other parameters:  $k_r = 10^{-13} \text{ m}^2$ ,  $S_\varepsilon = 10^{-10} \text{ Pa}^{-1}$ .



# Conclusion

- ▶ Algorithm of radial **hydraulic fracture growth** in 3D poroelastic medium is constructed
  - Simple to implement
  - Robust in wide parameters range
- ▶ Dimensionless complexes reflecting **diffusion regime** and **backstress** are considered. Critical values are estimated
- ▶ **Deformation** domination diffusion case is **investigated**